AMENDMENT(S) TO THE SPECIFICATION

The applicants note that the Examiner objects to the substitute specification filed February 24, 2003, stating the substitute specification has not been entered because it does not conform to 37 C.F.R. § 1.125(b). The applicants note that on page 3 at lines 10 through 11 of the February 24, 2003, Amendment/Submission, the applicants state that "the attached Substitute Specification (Appendix C) contains no new matter and meets the requirement of 37 C.F.R. § 1.125." The applicants again submit that the February 24, 2003, substitute specification includes no new matter.

The applicants assume that the February 24, 2003, substitute specification does conform to 37 C.F.R. § 1.125(b) and that the substitute specification has been entered. The following amendments, therefore, are made to the February 24, 2003, substitute specification.

Please replace the paragraph on page 9 at lines 8 through 23 of the February 24, 2003, substitute specification, with the following amended paragraph:

It is apparent from figures 2a3 and 2a4 that, under the influence of the circumferential force, the force distribution onto the rolling elements 14 of the roller-bearing arrangement 11 is greatest in the region of the outer surfaces 18 of the yoke half 4.1 and in the surface regions of the supporting surface 10 that point in the circumferential direction and are here designated 19. The forces here arise from the compressive stresses acting on the supporting surface 10, which in turn are determined by the axial load, bending and radial load. The circumferential force or tangential force on the rolling elements ~~11~~ <u>14</u> toward the supporting surface 10 is greatest in those regions which, viewed in the circumferential direction, based on the axis of symmetry S_{GM} of the yoke half 4.1, which extends perpendicularly to the axis of the bore, which corresponds to the journal axis Z1 of the journal 6 of the journal arrangement 5 mounted in the bore 9, are arranged symmetrically, a lifting of the rolling elements 14 is observable. This partial contact of the rolling elements 14 on the running tracks, or on the elements forming the running tracks for the rolling elements 14, in particular on the outer ring 13 and the inner ring 15, results in a reduction of the bearing capacity of the entire roller-bearing arrangement 11. The nonuniform stresses on the bearing connection elements, in particular the bearing part 8 of the yoke half 4.1, result in corresponding fatigue phenomena in the highly stressed regions.

Please replace the paragraph beginning on page 9 at line 24 and ending on page 10 at line 13 of the February 24, 2003, substitute specification, with the following amended paragraph:

According to the invention, therefore, a yolk half 4.1a is provided, including a supporting surface 10a, a bearing part 8a, a leg member 7a, an outer surface 18a, an inner surface 22a, and a bore 9a. It is proposed that the supporting surface 10a, which is formed by the bore 9a, be provided with recesses 20 locally in the regions which support the most highly stressed rolling elements 14 of the roller-bearing arrangement 11. For reasons of clarification, the yoke half 4.1a is reproduced in section in the case illustrated, while the local recess 20 made in the supporting surface 10a is reproduced with double hatching. It becomes apparent from this that the local recess 20 extends substantially from the outer surface 18a of the yoke half 4.1a toward the pivot axis parallel to the journal axis Z1, preferably, as shown in Figure 1a, over the entire extent of the bore 9a in the direction parallel to the journal axis Z1. Furthermore, the recess 20 extends in the circumferential direction, in other words in the radial direction based on the journal axis Z1 viewed in the bore 9a. The extent in the circumferential direction occurs here via the extent of different size toward the pivot axis parallel to the journal axis Z1. In accordance with the load arising according to Figures 2a3 and 2a4 in a conventional embodiment with cylindrical bore 9, the recess 20 as illustrated in Figure 1b possesses the maximum dimensions in terms of depth t and extent in the circumferential direction, here designated as width b, in the region of the outer surface 18a of the yoke half 4.1a in the bore 9a. These dimensions diminish here in the direction of the pivot axis. The force distribution achievable in the bore with this supporting structure is shown in figures 2b1 and 2b2.

C2

Please replace the paragraph on page 11 at lines 18 through 20 of the February 24, 2003, substitute specification, with the following amended paragraph:

In accordance with still another exemplary articulated yoke of the present invention, the supporting surface ~~10~~ 10a and/or the surface of the supporting surface ~~10~~ 10a that can be described by the recess 20 are surface-treated.

C3

Please replace the paragraph on page 11 at lines 21 through 22 of the February 24, 2003, substitute specificati n, with the following amended paragraph:

In accordance with yet another exemplary articulated yoke of the present invention, the supporting surface ~~10~~ 10a and/or recess 20 are provided with a perforation.

C4

Please replace the paragraph on page 11 at lines 25 through 26 of the February 24, 2003, substitute specification, with the following amended paragraph:

In accordance with ~~yet another~~ an exemplary articulated yoke of the present invention, the bore ~~9~~ 9a is designed as a blind hole.

C5